

四层成层水域内波的研究¹

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摘要: 运用小振幅波理论研究了四层成层水域的内波运动, 给出了四层成层状态下的各界面波波面位移和各层速度势的解析表达式及各层深度平均流速分布和内波波频散关系, 并与三层成层水域内波的解析结果进行了比较。

关键词: 内波; 四层成层水域; 小振幅波理论

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长期以来, 人们对内波进行了广泛的研究, 如 Benjamin^[1], Benjamin^[2], Davis 等^[3], Ono^[4], Joseph^[5], Kubota 等^[6]。Stokes^[7]建立了两层海洋内波理论, Lamb^[8]详细描述了小振幅内波的特性, 而 Defant^[9]和 Benjamin^[11]分别研究了内长波和孤立波的相应特性。最近, Choi 等^[10]在上层流体厚度与特征波长相比是一小量假设下导出两层流体系统中二维弱非线性内波的一般演化方程, Choi 等^[11]在某一层流体厚度与特征波长相比是一小量假设下给出了两层流体系统中完全非线性内波的一般演化方程等。这些研究都是针对两层成层水域内波, 对于两层以上成层水域内波的研究, 目前结果较少, 章守宇和杨红^[12]研究了三层成层水域内波。但是在真实的海洋内部, 这种密度二层成层有时并不能很好地描述成层现象。例如在中纬度海区的对流层下方, 通常就存在着永久性温跃层, 在春夏季的成层期很容易与对流层以内的季节性成层构成多层成层; 另外, 水深较浅的沿岸养殖水域如内湾在成层期, 内波产生的海水混合弱化了密度的成层, 同时潮汐通过湾口不断与湾内水进行交换, 使得湾内水的密度垂直分布变得异常复杂。因此, 应用两层或三层成层的方法去近似, 势必不够准确。作者以小振幅波理论为基础, 就密度四层成层状态下的内波波动规律进行了一些研究, 并与三层成层水域内波的解析结果进行了比较。

1 数学模型

如图 1 所示, 我们考虑水深 H 为一常数, 密度

呈四层成层的流体。设流体为无粘不可压的, 且波动的振幅相对于波长很小, 即为小振幅波动, 同时设各层流体厚度相对于波长也很小, 并忽略地球旋转的影响。取静止水面向右为 x 轴正方向, 垂直向上为 z 轴正向。自水面而下, 成层流体厚度分别为 h_1, h_2, h_3 和 h_4 , 密度分别为 ρ_1, ρ_2, ρ_3 和 ρ_4 。不同的密度流体之间构成的各界面水深坐标则分别为 z_0, z_1, z_2, z_3 和 z_4 , $z_0=0$ 表示水面, z_4 表示底面。假定流体是无旋的, 其速度可由势函数 $\Phi(x, z, t)$ 来表示为:

$$u = -\frac{\partial \Phi}{\partial x}, \quad w = -\frac{\partial \Phi}{\partial z} \quad (1)$$

这里 u 和 w 分别是水粒子在 x, z 方向的运动速度。对于第 $i(i=1, 2, 3, 4)$ 层流体, 有连续方程

$$\frac{\partial u_i}{\partial x} + \frac{\partial w_i}{\partial z} = 0, \quad i=1, 2, 3, 4 \quad (2)$$

将 (1) 代入 (2), 得

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$$\frac{\partial^2 \Phi_i}{\partial x^2} + \frac{\partial^2 \Phi_i}{\partial z^2} = 0, \quad i=1,2,3,4 \quad (3)$$

$$\left. \begin{aligned} p_1 &= \rho_1 \frac{\partial \Phi_1}{\partial t} - \rho_1 g z, & (z_1 + \eta_1 \leq z \leq z_0) \\ p_2 &= \rho_2 \frac{\partial \Phi_2}{\partial t} - \rho_2 g(z - z_1) + \rho_1 g h_1, & (z_2 + \eta_2 \leq z \leq z_1 + \eta_1) \\ p_3 &= \rho_3 \frac{\partial \Phi_3}{\partial t} - \rho_3 g(z - z_2) + \rho_1 g h_1 + \rho_2 g h_2, & (z_3 + \eta_3 \leq z \leq z_2 + \eta_2) \\ p_4 &= \rho_4 \frac{\partial \Phi_4}{\partial t} - \rho_4 g(z - z_3) + \rho_1 g h_1 + \rho_2 g h_2 + \rho_3 g h_3, & (z_4 \leq z \leq z_3 + \eta_3) \end{aligned} \right\} \quad (4)$$

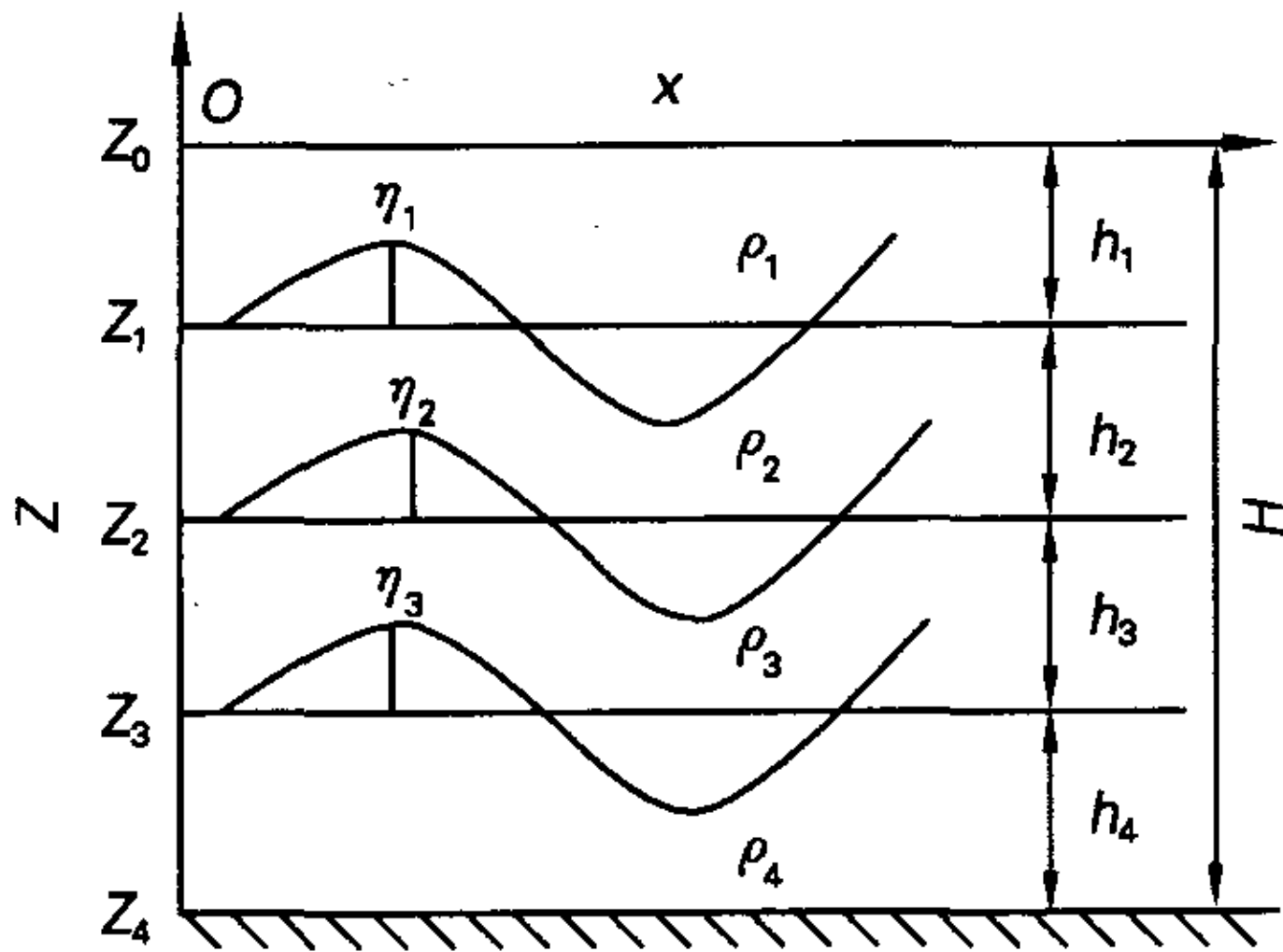


图1 四层成层水域的结构及内波示意

Fig.1 Schematic view of four-layer stratified fluid and internal wave

其中, g 为重力加速度。设 η_1, η_2 和 η_3 分别表示界面 1, 2, 3 处波动的波面位移, 显然对于界面 1, 2, 3, 有

$$\left. \begin{aligned} p_1 \Big|_{z=z_1+\eta_1} &= p_2 \Big|_{z=z_1+\eta_1}, & p_2 \Big|_{z=z_2+\eta_2} &= p_3 \Big|_{z=z_2+\eta_2}, \\ p_3 \Big|_{z=z_3+\eta_3} &= p_4 \Big|_{z=z_3+\eta_3} \end{aligned} \right\}$$

于是可得对于界面 1, 2, 3 的动力学条件

$$\left. \begin{aligned} \rho_1 \left[\frac{\partial \Phi_1}{\partial t} - g \eta_1 \right] &= \rho_2 \left[\frac{\partial \Phi_2}{\partial t} - g \eta_1 \right], & z &= z_1 + \eta_1 \\ \rho_2 \left[\frac{\partial \Phi_2}{\partial t} - g \eta_2 \right] &= \rho_3 \left[\frac{\partial \Phi_3}{\partial t} - g \eta_2 \right], & z &= z_2 + \eta_2 \\ \rho_3 \left[\frac{\partial \Phi_3}{\partial t} - g \eta_3 \right] &= \rho_4 \left[\frac{\partial \Phi_4}{\partial t} - g \eta_3 \right], & z &= z_3 + \eta_3 \end{aligned} \right\} \quad (5)$$

假设水域下底面不可渗透, 上表面为刚性边界, 则有

$$-\frac{\partial \Phi_4}{\partial z} \Big|_{z=z_4} = 0, \quad \frac{\partial \Phi_1}{\partial z} \Big|_{z=0} = 0 \quad (6)$$

另外, 满足 (3) 的运动学边界条件为

式 (3) 即为流体关于速度势函数的连续方程, 且是 Laplace 方程。

设各层流体的动压力为 p_1, p_2, p_3 和 p_4 , 则有

$$\frac{\partial \eta_1}{\partial t} = -\frac{\partial \Phi_1}{\partial z} \Big|_{z=z_1+\eta_1}, \quad \frac{\partial \eta_1}{\partial t} = -\frac{\partial \Phi_2}{\partial z} \Big|_{z=z_1+\eta_1} \quad (7-1)$$

$$\frac{\partial \eta_2}{\partial t} = -\frac{\partial \Phi_2}{\partial z} \Big|_{z=z_2+\eta_2}, \quad \frac{\partial \eta_2}{\partial t} = -\frac{\partial \Phi_3}{\partial z} \Big|_{z=z_2+\eta_2} \quad (7-2)$$

$$\frac{\partial \eta_3}{\partial t} = -\frac{\partial \Phi_3}{\partial z} \Big|_{z=z_3+\eta_3}, \quad \frac{\partial \eta_3}{\partial t} = -\frac{\partial \Phi_4}{\partial z} \Big|_{z=z_3+\eta_3} \quad (7-3)$$

2 理论分析

由方程 (3), 势函数 Φ_i ($i=1,2,3,4$) 可取为下列形式

$$\Phi_i = Z_i(z) \cos(kx - \omega t), \quad i=1,2,3,4 \quad (8)$$

式中, ω 为内波的角频率, k 为波数, t 为时间。将 (8) 代入 (3), 可得

$$\frac{\partial^2 Z_i(z)}{\partial z^2} - k^2 Z_i(z) = 0, \quad i=1,2,3,4 \quad (9)$$

(9) 的一般解为

$$Z_i(z) = C_{i1} e^{kz} + C_{i2} e^{-kz}, \quad i=1,2,3,4 \quad (10)$$

式中 C_{i1}, C_{i2} ($i=1, 2, 3, 4$) 为常数。

考虑到小振幅波特点, $\sinh k(h_i + \eta_i) \approx \sinh kh_i$ ($i=1,2,3$), 且 $\rho_1 / \rho_2 \approx 1, \rho_2 / \rho_3 \approx 1, \rho_3 / \rho_4 \approx 1$, 并令 $\varepsilon_1 = (\rho_2 - \rho_1) / \rho_2, \varepsilon_2 = (\rho_3 - \rho_2) / \rho_3, \varepsilon_3 = (\rho_4 - \rho_3) / \rho_4$ 。由 (4), (5) 可以得到

$$\left. \begin{aligned} \eta_1 &= A_1 \sin(kx - \omega t) \\ \eta_2 &= A_2 \sin(kx - \omega t) \\ \eta_3 &= A_3 \sin(kx - \omega t) \end{aligned} \right\} \quad (11)$$

其中,

$$\left. \begin{aligned} A_1 &= \frac{\omega}{\varepsilon_1 g} [(C_{21} - C_{11})e^{kz_1} + (C_{22} - C_{12})e^{-kz_1}] \\ A_2 &= \frac{\omega}{\varepsilon_2 g} [(C_{31} - C_{21})e^{kz_2} + (C_{32} - C_{22})e^{-kz_2}] \\ A_3 &= \frac{\omega}{\varepsilon_3 g} [(C_{41} - C_{31})e^{kz_3} + (C_{42} - C_{32})e^{-kz_3}] \end{aligned} \right\} \quad (12)$$

$$\left. \begin{aligned} \Phi_1 &= -\frac{\omega A_1 \cosh kz}{k \sinh kh_1} \cos(kx - \omega t), & (z_1 + \eta_1 \leq z \leq z_0) \\ \Phi_2 &= \frac{\omega A_1 \cosh k(z - z_2) - A_2 \cosh k(z - z_1)}{k \sinh kh_2} \cos(kx - \omega t), & (z_2 + \eta_2 \leq z \leq z_1 + \eta_1) \\ \Phi_3 &= \frac{\omega A_2 \cosh k(z - z_3) - A_3 \cosh k(z - z_2)}{k \sinh kh_3} \cos(kx - \omega t), & (z_3 + \eta_3 \leq z \leq z_2 + \eta_2) \\ \Phi_4 &= \frac{\omega A_3 \cosh k(z - z_4)}{k \sinh kh_4} \cos(kx - \omega t), & (z_4 \leq z \leq z_3 + \eta_3) \end{aligned} \right\} \quad (13)$$

再将计算所得 $C_{11}, C_{12}, C_{21}, C_{22}, C_{31}, C_{32}, C_{41}, C_{42}$ 代入 (12), 并考虑到各层流体厚度相对于波长很小, 即 $\sinh kh_i \approx kh_i$, 整理可得关于界面振幅的三元方程组

$$\left. \begin{aligned} A_1 \left(\frac{\varepsilon_1 g h_2}{c^2} - \frac{h_1 + h_2}{h_1} \right) + A_2 &= 0 \\ A_1 + A_2 \left(\frac{\varepsilon_2 g h_2}{c^2} - \frac{h_2 + h_3}{h_3} \right) + \frac{h_2}{h_3} A_3 &= 0 \\ A_2 + A_3 \left(\frac{\varepsilon_3 g h_3}{c^2} - \frac{h_3 + h_4}{h_4} \right) &= 0 \end{aligned} \right\} \quad (14)$$

这里, $c = \omega/k$ 为波速。由 (14) 消去 A_1, A_2 , 和 A_3 可得

$$\left(\frac{\varepsilon_1 g h_2}{c^2} - \frac{h_1 + h_2}{h_1} \right) \left(\frac{\varepsilon_2 g h_2}{c^2} - \frac{h_2 + h_3}{h_3} \right) \left(\frac{\varepsilon_3 g h_3}{c^2} - \frac{h_3 + h_4}{h_4} \right) - \frac{h_2}{h_3} \left(\frac{\varepsilon_1 g h_2}{c^2} - \frac{h_1 + h_2}{h_1} \right) - \left(\frac{\varepsilon_3 g h_3}{c^2} - \frac{h_3 + h_4}{h_4} \right) = 0 \quad (15)$$

上式即为密度四层成层时的内波频散关系。由于 (15) 是 c^2 的三次代数方程, 因此, 波速 c 一般有三个解 c', c'', c''' , 这些解分别对应于密度四层成层内波的三种模态, 令 $c' > c'' > c'''$, 则可以称 c' 对应的模态为大波速模态, c''' 对应的为小波速模态。设界面振幅 A_1, A_2, A_3 之间存在关系

$$\left. \begin{aligned} A_2/A_1 &= \beta_1, \quad A_3/A_2 = \beta_2 \\ \beta_1, \beta_2 &\text{ 称为内波振幅比, 由 (14) 即可得} \end{aligned} \right\} \quad (16)$$

由 (11) 可知, 成层流体内部的界面依照正弦规律波动, A_1, A_2, A_3 分别为它们的振幅。

利用边界条件 (6) 和 (7), 并基于小振幅波理论, 由 (8), (10), (11), 解得各常数 $C_{11}, C_{12}, C_{21}, C_{22}, C_{31}, C_{32}, C_{41}, C_{42}$, 得到密度四层成层状态时的速度势函数为

$$\left. \begin{aligned} \frac{\varepsilon_1 g h_2}{c^2} - \frac{h_1 + h_2}{h_1} + \beta_1 &= 0 \\ \frac{1}{\beta_1} + \left(\frac{\varepsilon_2 g h_2}{c^2} - \frac{h_2 + h_3}{h_3} \right) + \frac{h_2}{h_3} \beta_2 &= 0 \\ \frac{1}{\beta_2} + \left(\frac{\varepsilon_3 g h_3}{c^2} - \frac{h_3 + h_4}{h_4} \right) &= 0 \end{aligned} \right\} \quad (17)$$

因此, 如果由 (15) 求得波速 c , 则由 (17) 即可求得内波振幅比 β_1, β_2 , 从而就可以讨论界面波波形。下面给出密度四层成层时各层流体的深度平均水平流速

$$\left. \begin{aligned} \bar{u}_1 &= \frac{1}{h_1} \int_{z_1}^{z_0} -\frac{\partial \Phi_1}{\partial x} dz = -c \frac{1}{h_1} A_1 \sin(kx - \omega t) \\ \bar{u}_2 &= \frac{1}{h_2} \int_{z_2}^{z_1} -\frac{\partial \Phi_2}{\partial x} dz = c \frac{1 - \beta_1}{h_2} A_1 \sin(kx - \omega t) \\ \bar{u}_3 &= \frac{1}{h_3} \int_{z_3}^{z_2} -\frac{\partial \Phi_3}{\partial x} dz = c \frac{1 - \beta_2}{h_3} A_2 \sin(kx - \omega t) \\ \bar{u}_4 &= \frac{1}{h_4} \int_{z_4}^{z_3} -\frac{\partial \Phi_4}{\partial x} dz = c \frac{\beta_2}{h_4} A_2 \sin(kx - \omega t) \end{aligned} \right\} \quad (18)$$

式 (18) 描述了界面波形与流速的关系。由 (15), (17), (18) 即可讨论四层成层水域内波的波形及流况。为简单起见, 这里仅以一特例来作一些分析。取

$$h_1 = h_2 = h_3 = h_4 = 1, \quad \varepsilon_1 = \varepsilon_2 = \varepsilon_3 = \varepsilon_4 = \varepsilon = 0.001 \quad (19)$$

将 (19) 代入 (15), 可得

$$c'^2 = \frac{\varepsilon g}{2 - \sqrt{2}}, \quad c''^2 = \frac{\varepsilon g}{2}, \quad c'''^2 = \frac{\varepsilon g}{2 + \sqrt{2}} \quad (20)$$

将 (19) 代入 (17), 可得
当内波以 c' 对应的大波速模态传播时

$$\beta_1 = \sqrt{2}, \quad \beta_2 = 1/\sqrt{2} \quad (21)$$

当内波以 c'' 对应的模态传播时

$$\beta_1 = 0, \quad 1/\beta_2 = 0 \quad (22)$$

当内波以 c''' 对应的小波速模态传播时

$$\beta_1 = -\sqrt{2}, \quad \beta_2 = -1/\sqrt{2} \quad (23)$$

分析:

当内波以大波速 c' 对应的大波速模态传播时, 由于 β_1, β_2 均大于 0, 故界面 1, 2, 3 的振动呈同相位, 此时上面两层流体粒子平均运动方向相同, 下面两层流体粒子平均运动方向相同, 但上面两层流体粒子平均运动方向与下面两层流体粒子平均运动方向相反(图 2a), 这种情形类似于密度三层成层流体^[12]

大波速模态的情形。

当内波以波速 c'' 对应模态传播时, 此时 $\beta_1=0$, 从而 $A_2=0$ 由 (14) 可得 $A_1=-A_3$, 故界面 1, 3 的振动呈逆相位, 界面 2 的振幅为 0。由(18), 有

$$\bar{u}_1 = -\bar{u}_2, \quad \bar{u}_2 = \bar{u}_3, \quad \bar{u}_1 = \bar{u}_4$$

即上面两层流体粒子平均运动方向相反, 下面两层流体粒子平均运动方向也相反, 中间两层流体粒子平均运动方向相同(图 2b), 此情形就是密度三层成层流体^[12]小波速模态的情形。

当内波以小波速 c''' 对应的小波速模态传播时, 由于 β_1, β_2 均小于 0, 故界面 1, 3 的振动呈同相位, 而 1, 2 及 2, 3 的振动分别呈逆相位, 此时相邻的两层流体粒子平均运动方向都相反(图 2c), 此情形类似于密度三层成层流体^[12]小波速模态的情形。

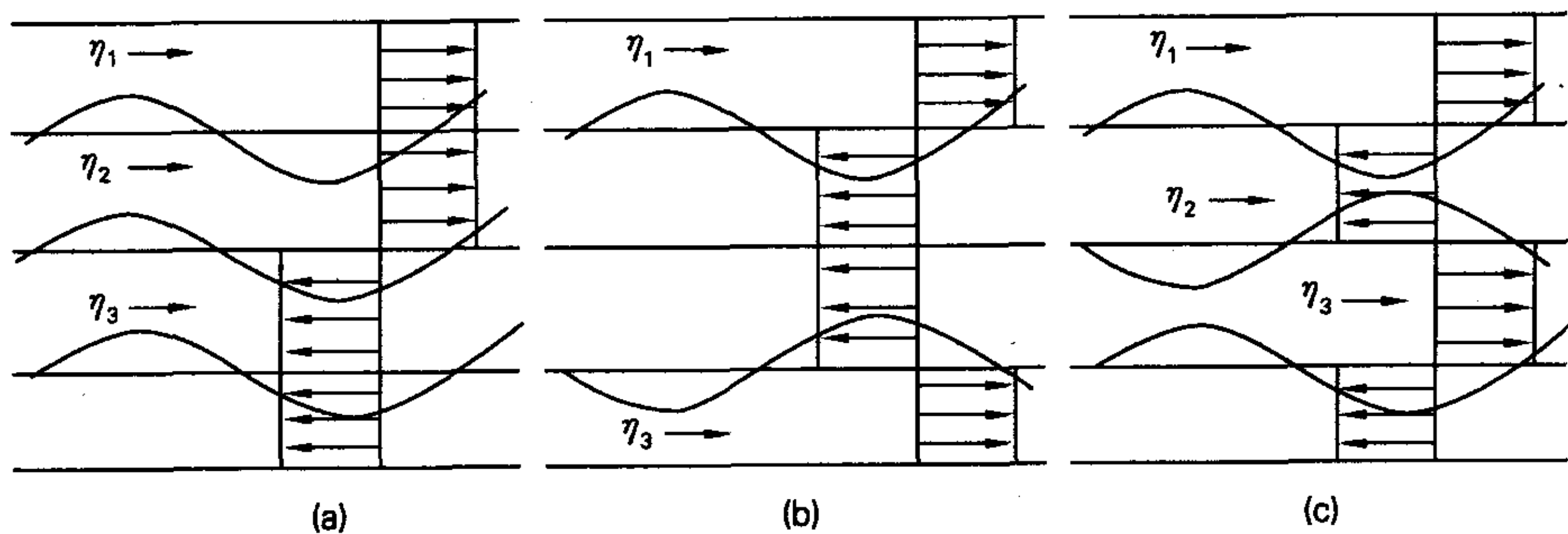


图 2 四层成层水域的内波波形及流况示意

Fig. 2 Phase of interfacial wave and its flow characters in four-layer stratified fluid

3 结论

利用小振幅波理论, 研究了四层成层水域内波波动规律, 给出了各层波动解的解析表达式, 并以实际观测到的内波为例, 与三层成层水域内波理论作了比较, 结果如下:

在小振幅波理论基础下, 四层成层水域的内波有三种模态, 大波速模态波动时, 其流况及界面波动特征与三层成层状态大波速模态时的情形类似; 其它两种波速模态波动时, 其流况及界面波动特征与三层成层状态小波速模态时的情形类似。

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(上接第 41 页)

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Study on internal wave in four-layer stratified fluid

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Abstract: In this paper, motions of internal waves in four-layer stratified fluid were investigated, and solutions of the elevations of the interfacial waves and the associated velocity potentials were presented based on small amplitude wave theory. Patterns of distribution of mean velocity due to the waves and its dispersion relationship were derived, and they are compared with the analytic results of the study on internal wave in three-layer stratified fluid.

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