

台湾以东海域黑潮热结构的 一个简单模型*

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多年来,对紧邻台湾东侧的黑潮区域,已积累了一定数量的温、盐度观测资料。从实测的水温垂直断面图上,可以看出该区域的水温分布有如下特点。

1. 在水平方向上:水温自西向东逐渐增加,其最大值在离岸70km左右(即所谓“热核”所在处);再向东温度开始递减,其低温区呈现在“热核”东侧。图1示台湾以东海域100m层的水温分布^[1],可看出温度水平分布的这些特点。

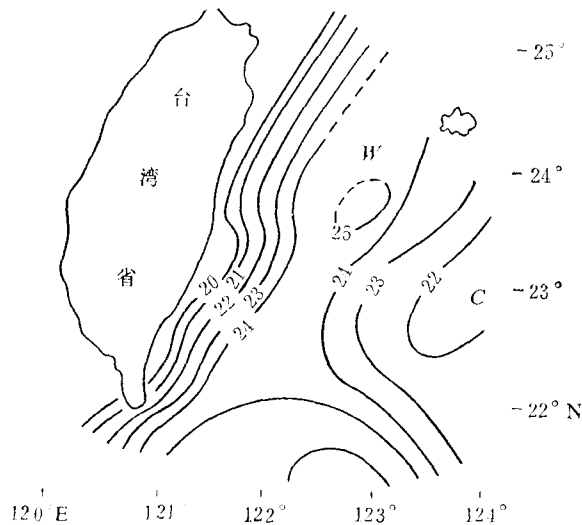


图1 台湾省以东海域100m层的水温(°C)分布
(1966.3—4,“阳明”号船调查^[1])

2. 在垂直方向上:近表层(海面以下约100m)温度呈均匀分布,强温跃层往往出现在海面以下150—300m内。其温度变化经常在10°C左右,有时甚至可达十几度。跃层以下的温度则随着深度的增加而缓慢递减,其递减率越来越小,至1000m左右下降到4°C附近(参看图3)。图3给出了台湾以东(北纬23°45′断面上)011站的温度垂直分布。

3. 温度纬向分布的不均匀性(即温度水平梯度):在离岸方向上随着距离的增加而减

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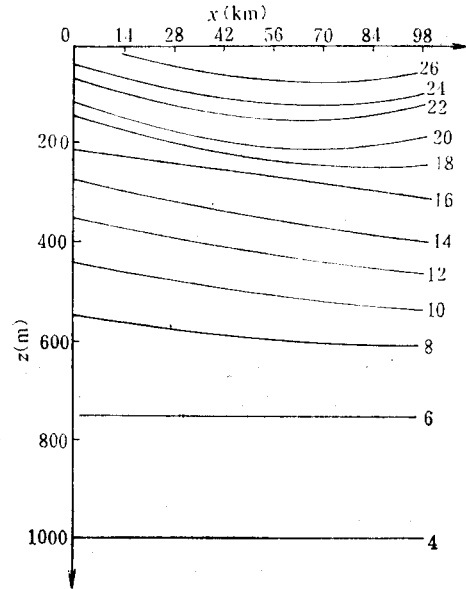


图2 台湾省以东海域(23°45'N)垂直断面水温(°C)分布
(1966.3—4,“阳明”号船调查)

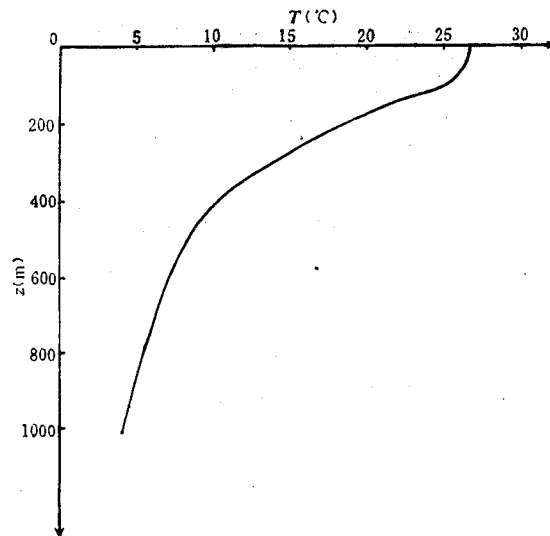


图3 台湾省以东海域(23°45'N, 011站)水温(°C)垂直分布
(1966.3.14,“阳明”号船调查)

小;在垂直方向上则随着深度的增加而递减。图2表明台湾以东海域北纬23°45'的垂直断面上温度分布,等温线在离岸70km附近下凹的现象,被局限在离海面250m以上的水层范围。250m层以下这种下凹的趋势已不甚明显,等温线只是自海岸向外海单调下倾,其倾斜程度随着深度的增加逐步衰减,至800—1000m左右,等温线已几乎呈水平分布。

本文试图建立一个台湾以东海域黑潮热结构的简单模型。当给定海区边界上的温度

分布后,海区内部的热结构主要取决于垂直热对流和涡动热扩散之间的相互平衡。模式解所确定的温度场主要特征和上述定性分析所得的结论是一致的。

一、控制方程和边界条件

本文所研究的黑潮区域,水深均大于 800—1000m。取笛卡儿坐标系, x 轴向东; y 轴向北; z 轴垂直向上; 坐标原点选在水深 1000m 处。研究海区的西边界位于台湾岛东侧附近的垂直断面上,东边界位于离岸 600km 以远处或开阔大洋;南边界和北边界假定在相当远处。运动假设为稳态的,不考虑柯氏参量随纬度的变化;略去水平涡动混合所导致的动量输送;不考虑表面风应力。运动方程取准地转平衡和静力平衡。根据实测资料分析,可以取 u 方程为地转方程;在 v 方程中考虑到垂直涡动粘性项,并采用 Boussinesq 近似。在热方程中,仅保留垂直热对流和涡动热扩散。为使热方程线性化,本文采用了类似于 Oseen 型的近似处理^[2],于是控制方程取为:

$$-fv' = -\frac{1}{\rho_0} \frac{\partial p'}{\partial x'}, \quad (1)$$

$$fu' = -\frac{1}{\rho_0} \frac{\partial p'}{\partial y'} + \frac{\partial}{\partial z'} \left(A_v \frac{\partial v'}{\partial z'} \right), \quad (2)$$

$$0 = -\frac{1}{\rho_0} \frac{\partial p'}{\partial z'} - g \frac{\Delta \rho}{\rho_0}, \quad (3)$$

$$\frac{\partial u'}{\partial x'} + \frac{\partial v'}{\partial y'} + \frac{\partial w'}{\partial z'} = 0, \quad (4)$$

$$\rho' = \rho_0 [1 - \alpha(T' - T_0)], \quad (5)$$

$$w' \frac{\partial T'}{\partial z'} = k_H \nabla'^2 T' + k_v \frac{\partial^2 T'}{\partial z'^2}. \quad (6)$$

其中 u', v', w' 分别为坐标轴 x', y', z' 方向上的速度分量。右上角上的小撇表示有维量, T' 被认为是“等效”温度,它是实际温度和盐度的线性组合。也就是说盐度效应是通过等效温度来体现的^[3]。 ρ' 和 p' 为密度和压力; ρ_0 和 T_0 为特征海水密度和海水温度; α 为等效热膨胀系数; $\Delta \rho$ 表示在温度 T' 时的密度 ρ' 和 ρ_0 之差; A 和 k 表示流体运动的涡动粘性系数和涡动热扩散系数,由于水平方向和垂直方向涡动特性的量级相差很大,分别以脚标 H 和 v 加以区别,且假设为常值。 ∇'^2 为二维拉氏算子,由于采用了类似于 Oseen 型的近似^[3], 其对流项的垂直温度梯度 $\frac{\partial T'}{\partial z'}$ 将用常数 $H^{-1} \Delta T$ 来代替。引入无量纲变量:

$$\left. \begin{aligned} \langle u', v' \rangle &= \frac{\alpha g H \Delta T}{f L} \langle u, v \rangle \\ w' &= \frac{\alpha g H^2 \Delta T}{f L^2} w \\ p' &= \rho_0 + [\rho_0 \alpha g \Delta T H] p \\ T' &= T_0 + (\Delta T) T \\ \langle x', y' \rangle &= L \langle x, y \rangle \\ z' &= H z \end{aligned} \right\} \quad (7)$$

其中 ΔT 是一个特征的温度差, H 和 L 分别为垂直和水平长度的特征值, p_0 视为海面大气压力, 取为常值。将 (7) 式代入 (1)–(6) 式可得无量纲化的控制方程:

$$v = \frac{\partial p}{\partial x}, \quad (8)$$

$$u = -\frac{\partial p}{\partial y} + 1K_v \frac{\partial^2 v}{\partial z^2}, \quad (9)$$

$$T = \frac{\partial p}{\partial z}, \quad (10)$$

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0, \quad (11)$$

$$\mathcal{E}w = K_H \nabla^2 T + K_v \frac{\partial^2 T}{\partial z^2}. \quad (12)$$

其中:

$$1K_v = \frac{A_v}{fH^2}; \quad \mathcal{E} = \frac{\alpha g H \Delta T}{fL^2};$$

$$K_H = \frac{k_H}{fL^2}; \quad K_v = \frac{k_v}{fH^2}.$$

∇^2 为二维无量纲水平拉普拉斯算子。

考虑到上述的无量纲化处理, 问题已归结为南北方向(经向)为无限长, 横截面为单位深度和单位宽度的海域内等效温度场和流场的模式解。

在高度层化的流体中, 当垂直涡动粘性和垂直涡动扩散性均取为常值时, 温度场和流场的垂直结构, 将主要取决于垂直边界的选择^[2]。本文讨论的是紧邻台湾岛东侧的黑潮区域(该区域仅是研究海域西边界附近极为狭窄的一条带), 因此, 海区西边界条件的选择是至关重要的。取 $x = 0$ 处(黑潮主轴)的温度边界条件为:

$$T' = T'_a + \nu e^{\delta z'} \left(\frac{z' - \sigma}{D} \right)^{\frac{1}{2}}. \quad (13)$$

(13) 式表示强温跃层位于 $z' = \sigma$ 附近, 温跃层厚度近似取为 $2D$ 。在 $\sigma + D \leq z' \leq H$ 内, 为近表层, 其温度垂直分布近似均匀; 在 $\sigma - D \leq z' \leq \sigma + D$ 内, 为温跃层所在的区域, 温度垂直梯度自 $z' = \sigma + D$ 向下急剧增加, 至 $z' = \sigma$ 处达最大值, 然后向下便急剧减小; 在 $0 \leq z' \leq \sigma - D$ 内, 温度向下缓慢递减。公式 (13) 所给出的温度垂直分布模式, 从本文所举的实例来看, 较好地模拟了黑潮主轴的温度垂直结构。

海区东边界 ($x = L$), 由于对黑潮区域影响较小, 其边界条件可近似取为:

$$\frac{\partial T'}{\partial x'} = 0. \quad (x = L) \quad (14)$$

海面 ($z' = H$ 处) 的边界条件:

$$A_v \frac{\partial v'}{\partial z'} = 0, \quad w' = 0, \quad (15)$$

$$T' = \tilde{T}' + T'_1 e^{-\varepsilon x'} \sin \frac{2n\pi}{L} x'. \quad (16)$$

海区下边界 ($z' = 0$) 处的边界条件:

$$T' = T_0, \quad (17)$$

上述边界条件的无量纲形式分别为:

$$x = 0 \quad T = I + q_0^* e^{\beta^* z} (z - J^*)^{\frac{1}{3}}, \quad (18)$$

$$x = 1 \quad \frac{\partial T}{\partial x} = 0, \quad (19)$$

$$z = 0 \quad T = 0, \quad (20)$$

$$z = 1 \quad \frac{\partial v}{\partial z} = 0, \quad w' = 0 \quad T = \tilde{T} + T_1 e^{-\mu x} \sin Nx_0. \quad (21)$$

其中要求

$$I + q_0^* e^{\beta^*} (1 - J^*)^{\frac{1}{3}} = \tilde{T}$$

以满足 $x = 0, z = 1$ 处的匹配条件。

二、温度场的解

由边界条件 (21), 利用方程 (8) 和 (11) 可得:

$$w = -1K_v \frac{\partial^2 T}{\partial x^2}, \quad (22)$$

代入 (12) 式, 则 T 方程为:

$$(K_H + \varepsilon 1K_v) \frac{\partial^2 T}{\partial x^2} + K_H \frac{\partial^2 T}{\partial y^2} + K_v \frac{\partial^2 T}{\partial z^2} = 0. \quad (23)$$

由于本文假设南边界和北边界在相当远处, 则沿 y 方向的速度涡动扩散可忽略不计, 公式 (23) 可化简为:

$$\lambda^2 \frac{\partial^2 T}{\partial x^2} + K_v \frac{\partial^2 T}{\partial z^2} = 0. \quad (24)$$

这里:

$$\lambda^2 = K_H + \varepsilon 1K_v. \quad (25)$$

若取所考虑的各参数量级分别为:

$$\begin{aligned} \alpha &= 10^{-4} & g &= 10^3 & f &= 10^{-4} \\ L &= 10^8 & H &= 10^5 & \Delta T &= 10^1 \\ k_H &= 10^6 & k_v &= 10^1 & A_v &= 10^1 \end{aligned}$$

则方程 (24) 中的系数 λ^2 和 K_v 均为小量, 其量级为:

$$\lambda^2 = 10^{-7}, \quad K_v = 10^{-5}.$$

引进拉伸变换:

$$\zeta = K_v^{-\frac{1}{2}}(1 - z), \quad (26)$$

则所解的边值问题为:

$$\frac{\partial^2 T}{\partial \zeta^2} + \lambda^2 \frac{\partial^2 T}{\partial x^2} = 0. \quad (27)$$

$$x = 0 \quad T = I - q_0 e^{-\beta \zeta} [\zeta - J]^{\frac{1}{3}}, \quad (28)$$

$$x = 1 \quad \frac{\partial T}{\partial x} = 0, \quad (29)$$

$$\zeta = 0 \quad T = \tilde{T} + T_1 e^{-\mu x} \sin Nx, \quad (30)$$

$$\zeta \rightarrow \infty \quad T, \frac{\partial T}{\partial \zeta} \rightarrow 0. \quad (31)$$

因为参数 λ^2 为小量, 可以采用边界层技术, 用星号(*)来表示富里哀正弦变换, 定义 T^* 为:

$$T^*(x, \eta) = \sqrt{\frac{2}{\pi}} \int_0^\infty T(x, \zeta) \sin \eta \zeta d\zeta, \quad (32)$$

则 T^* 所满足的方程和边界条件是:

$$\lambda^2 \frac{\partial^2 T^*}{\partial x^2} - \eta^2 T^* + \eta(\tilde{T} + T_1 e^{-\mu x} \sin Nx) = 0, \quad (33)$$

$$x = 0 \quad T^* = \frac{I}{\eta} - \frac{I \cos K_v^{-\frac{1}{2}} \eta}{\eta}$$

$$- q_0 e^{-\beta T} \frac{\Gamma\left(\frac{4}{3}\right)}{(\beta^2 + \eta^2)^{\frac{2}{3}}} \sin \left[J\eta + \frac{4}{3} \operatorname{tg}^{-1} \frac{\eta}{\beta} \right], \quad (34)$$

$$x = 1 \quad \frac{\partial T^*}{\partial x} = 0. \quad (35)$$

求得定解问题(33)–(35)的解为:

$$\begin{aligned} T^* = & \tilde{T} \frac{1}{\eta} + \frac{T_1 e^{-\mu x} \sin Nx}{2} \left(\frac{p + \eta}{(p + \eta)^2 + q^2} - \frac{p - \eta}{(p - \eta)^2 + q^2} \right) \\ & + \frac{T_1 q e^{-\mu x} \cos Nx}{2} \left(\frac{1}{(p + \eta)^2 + q^2} - \frac{1}{(p - \eta)^2 + q^2} \right) \\ & + \frac{\operatorname{ch}(1-x) \frac{\eta}{\lambda}}{\operatorname{ch} \frac{\eta}{\lambda}} \left\{ I \frac{1}{\eta} - \frac{I \cos K_v^{-\frac{1}{2}} \eta}{\eta} \right. \\ & - q_0 e^{-\beta J} \frac{\Gamma\left(\frac{4}{3}\right)}{(\beta^2 + \eta^2)^{\frac{2}{3}}} \sin \left[J\eta + \frac{4}{3} \operatorname{tg}^{-1} \frac{\eta}{\beta} \right] - \tilde{T} \frac{1}{\eta} \\ & \left. - \frac{T_1 q}{2} \left(\frac{1}{(p^2 + \eta^2)^2 + q^2} - \frac{1}{(p^2 - \eta^2)^2 + q^2} \right) \right\} \\ & + \frac{\operatorname{sh} \frac{\eta}{\lambda} x}{\operatorname{ch} \frac{\eta}{\lambda}} \left\{ \frac{T_1 p q e^{-\mu}}{2\eta} \left(\frac{1}{(p^2 + \eta^2)^2 + q^2} - \frac{1}{(p^2 - \eta^2)^2 + q^2} \right) \right. \\ & \left. - \frac{T_1 q e^{-\mu}}{2\eta} \left(\frac{p + \eta}{(p^2 + \eta^2)^2 + q^2} - \frac{p - \eta}{(p^2 - \eta^2)^2 + q^2} \right) \right\}. \quad (36) \end{aligned}$$

其中 $\lambda^2 \mu^2 = p^2$, $\lambda^2 N^2 = q^2$, 而相应的

$$\begin{aligned}
 T = & \tilde{T} + T_1 e^{-A\zeta - \mu x} \sin(Nx - B\zeta) \\
 & - \frac{2\lambda T_1 e^{-\mu}(pB + qA) \sin \frac{\pi}{2} x}{A^2 + B^2} \int_0^\infty \frac{\operatorname{sh} \frac{\pi \lambda}{2} \xi}{\operatorname{ch} \pi \lambda \xi + \cos \pi x} d\xi \\
 & + [I - q_0 e^{-\beta \zeta} (\zeta - J)]^{\frac{1}{2}} - \tilde{T} + T_1 e^{-A\zeta} \sin B\zeta \\
 & * \left(-\frac{\lambda^2}{8\pi} \right)^{\frac{1}{2}} \left[\phi \left(1 - \frac{x - i\lambda \zeta}{4} \right) - \phi \left(1 - \frac{x + i\lambda \zeta}{4} \right) \right. \\
 & \left. + \phi \left(\frac{1}{2} + \frac{x + i\lambda \zeta}{4} \right) - \phi \left(\frac{1}{2} + \frac{x - i\lambda \zeta}{4} \right) - \frac{2\pi \operatorname{ish} \lambda \pi \zeta}{\operatorname{ch} \lambda \pi \zeta + \cos \pi(1-x)} \right]. \quad (37)
 \end{aligned}$$

其中:

$$\begin{aligned}
 A &= \sqrt{\frac{\sqrt{(q^2 - p^2)^2 + 4p^2 q^2} + (q^2 - p^2)}{2}}, \\
 B &= \sqrt{\frac{\sqrt{(q^2 - p^2)^2 - 4p^2 q^2} - (q^2 - p^2)}{2}}.
 \end{aligned}$$

表达式 (37) 即是本文研究海区的无量纲温度场 $T(x, z)$ 的模式解。利用 (37) 式可以绘出纬向断面上温度的垂直断面图。由于本文关心的是紧贴西边界附近的黑潮区域, 因此图 4 只给出了离岸 100km 范围内的温度垂直剖面图。比较图 2 和图 4, 可以明显看出两者相当一致。图 4 表明: 在离岸 70km 的范围内, 等温线自西向东下倾, 其斜度随着深度的增加而递减。水温最高的地方在离岸 70km 附近, 再向东至离岸 100km 的范围内, 等温线在 400m 以上的水层中自西向东上倾; 离岸 100km 左右处呈现低温区域, 这些特点

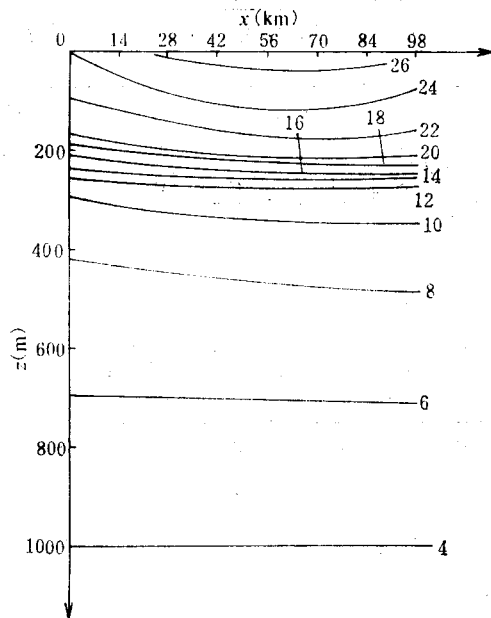


图 4 台湾省以东海域垂直断面水温(°C)分布
(理论模式计算结果)

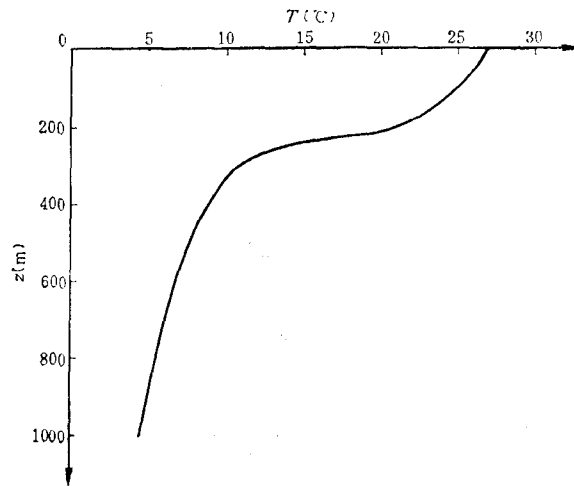


图5 台湾省以东海域(离岸42km处)水温($^{\circ}\text{C}$)垂直分布
(理论模式计算结果)

和图1所示的也很一致。图5根据表达式(37)给出了台湾省以东黑潮区域离岸42km处的水温垂直分布,强温跃层在水深150—300m范围内,温度差为 12°C 左右;和图3相比,两者十分接近。因此可以初步认为,黑潮区域的热结构主要取决于热方程(6),即垂直热对流和涡动热扩散取得平衡的结果。

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A SIMPLE MODEL FOR THE THERMAL STRUCTURE OF KUROSHIO EAST OF TAIWAN*

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ABSTRACT

It is assumed that the thermal structure within sea area is mainly dependent on the inter-equilibrium between vertical thermal convection and turbulent thermal diffusion if the distribution of temperature at the ocean boundary are given. A simple model of the thermal structure in the Kuroshio east of Taiwan is set up on the basis of the above assumption.

Suppose that the motion taken should be steady, without β -effect and wind stress, and the momentum transport caused by horizontal turbulent mixing should be neglected. The equations of motion are taken as the quasi-geostrophic balances and hydrostatic equilibrium, but the vertical turbulent viscosity term is added to V -equation. The Boussinesq approximation is utilized in the state equation. There are two terms (the vertical convection and diffusion) in the thermal equation. The approximate treatment similar to Oseen approximation is applied in this paper in order to make the thermal equation linearized.

In the strong stratified fluids, the vertical structures of the temperature and velocity fields mainly depend on the vertical boundary conditions because of the limitation of the constant coefficients of viscosity and diffusion. The Kuroshio area which we are interested in is adjacent to the east of Taiwan, which is only a strip of the west-boundary of this area. The vertical distribution of temperature is given as follows:

$$T = T^* + \alpha e^{\beta z} \left(\frac{z - a}{H} \right)^{\frac{1}{2}}. \quad (1)$$

This formula is taken as the thermal boundary condition to model the vertical distribution of temperature in the west-boundary of Kuroshio observed.

After the equation system is converted into nondimensional one, using non-dimensional variables, it is simplified into a two-dimensional T -equation, but it is worth noticing that its boundary condition at surface and west-boundary are nonhomogeneous. By means of the boundary layer technique of scale-transform and Fourier sin-transform, the T -equation has a solution as follows:

$$T = \tilde{T} + T_1 e^{-A\xi - \mu x} \sin(Nx - B\xi) \\ - \frac{2\lambda T_1 e^{-\mu}(pB + qA) \sin \frac{\pi}{2} x}{A^2 + B^2} \int_0^\infty \frac{\text{sh} \frac{\pi\lambda}{2} \xi}{\text{ch}\pi\lambda\xi + \cos\pi x} d\xi$$

* Contribution No. 1068 from the Institute of Oceanology, Academia Sinica.

$$\begin{aligned}
& + [I - q_0 e^{-B\zeta} (\zeta - T)^{\frac{1}{2}} - \tilde{T} + T_1 e^{-A\zeta} \sin B\zeta] * \left[\phi \left(1 - \frac{x - i\lambda\zeta}{4} \right) \right. \\
& - \phi \left(1 - \frac{x + i\lambda\zeta}{4} \right) + \phi \left(\frac{1}{2} + \frac{x + i\lambda\zeta}{4} \right) \\
& \left. - \phi \left(\frac{1}{2} + \frac{x - i\lambda\zeta}{4} \right) - \frac{2\pi i \operatorname{sh} \lambda\pi\zeta}{\operatorname{ch} \lambda\pi\zeta + \cos \pi(1-x)} \right] \left(-\frac{\lambda^2}{8\pi} \right)^{\frac{1}{2}} \quad (2)
\end{aligned}$$

in which

$$A = \sqrt{\frac{\sqrt{(q^2 - p^2)^2 + 4p^2q^2} + (q^2 - p^2)}{2}}, \quad B = \sqrt{\frac{\sqrt{(q^2 - p^2)^2 + 4p^2q^2} - (q^2 - p^2)}{2}}$$

$$p = \lambda \mu \quad \lambda = \sqrt{K_H + \varepsilon K_v}$$

$$q = \lambda N \quad \varepsilon = \frac{\alpha g H \Delta T}{f^2 L^2} \quad K_H = k_H / f L^2$$

$$\zeta = K_v^{-\frac{1}{2}} (1 - z) \quad K = A_v / f H^2 \quad K_v = k_v / f H^2$$

in which all other variables are pre-specified except x and z .

The main characteristics of the thermal structure in Kuroshio east of Taiwan as indicated by the model solution (2) is fairly consistent with the results observed in the area in March, 1966. Behaviours of both of their vertical temperature distribution plots are shown below:

1. Horizontally, the temperature gradually increased from the east coast of Taiwan eastwards to the place called "thermal nucleus", 70 km away from the coast, then gradually drops farther eastwards.

2. The vertical distribution of temperature was nearly homogeneous in the surface layer (from surface to 100 m depth). The strong thermocline used to appear in the 150—300 m depth and its variances in temperature were about 10°C or even more. The temperature under the thermocline decreased with the depth slowly and down to 4°C at about 1000 m.

3. The nonhomogeneity of latitudinal distribution of temperature (horizontal gradient of temperature) decreased with the off-shore distance and the depth. The "hol-low" phenomenon of isotherm near 70 km was only restricted to the upper layer (from surface to 250 m depth). This phenomenon appeared not to be obvious under 250 m-layer where isotherm just inclined downwards from the coast and its downwards slope decreased with the depth and within about 800—1000 m layer the isotherm was nearly horizontal.